NAS301H

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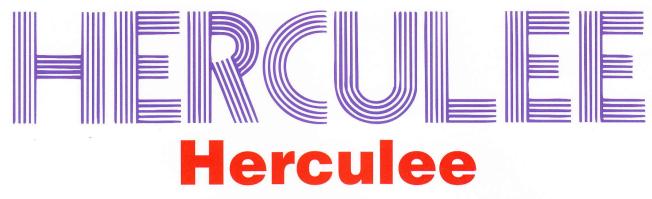
Asada Corporation is a specialized trading company for wires and strips such as steels, wires, piano wires, hard drawn steel wires, stainless steel wires etc. NAS

Herculee

Stainless steel wire for high-strength spring



Nippon Seisen Co., Ltd.



Stainless steel wire for high-strength spring

We respond to your variety of needs with our reliable technologies and flexible ideas.

With the recent trend toward downsizing products with low cost, materials having further strength and stronger ductility are being strongly called for, compared with the conventional stainless steel wire for spring.

In order to respond to such requirements, here, we have much pleasure in introducing our newly developed stainless steel wire for spring, that has super high-strength, excellent spring fatigue characteristic and permanent set resistance, as well as good coiling capability, compared with SUS304-WPB, by carefully examining specific composition, adopting our unique manufacturing method, and fully utilizing our long-cultivated technologies for manufacturing stainless steel wire for spring.

1. Characteristics

High-strength

Having tensile strength equivalent to that of piano wire Class A, and Class B (SWP-A, -B)

Excellent in fatigue strength

Enabling to design spring with higher stress compared with the conventional stainless steel wire for spring, and having excellent fatigue strength.

●Excellent in spring load characteristic

In the thin wire category, load characteristic of spring is at the equivalent level to piano wire that is more excellent than SUS304-WPB.

Excellent in permanent set resistance characteristic

Excellent in permanent set resistance when spring is repeatedly used.

2. Chemical composition

The following table 1 shows chemical composition standard for Herculee.

Table 1 Chemical composition

Unit: %

| | С | Si | Mn | P | S | Ni | Cr |
|----------|---------|---------|---------|---------|---------|--------|---------|
| Standard | 0.15 | 1.00 | 2.00 | 0.045 | 0.030 | 6.00 | 16.00 - |
| Standard | or less | - 8.00 | 18.00 |

Herculee belonging to SUS301 type of 17Cr-7Ni, basics of austenite-based stainless steel, is a steel type excellent in its work hardening characteristic which allows cold work-induced martensitic deformation to occur more easily compared with SUS304 of standard steel type 18Cr-8Ni.

3. Specifications

The following Table 2 shows specifications for Herculee.

Table 2 Specifications

| Standard wire | Tolerance for | Deviated | rance for Deviated Tensile strength Type of packing (inch) | | | | (1.) | | |
|---------------|---------------|--------------------------------------|--|------------|--------------|----------|-----------|------|------|
| diameter | wire diameter | diameter | Tensile strength (N/mm²) | Type of pa | cking (inch) | Standard | mass (kg) | | |
| (mm) | (mm) | (mm) | (14/111111-) | HNF | HUBNS | HNF | HUBNS | | |
| 0.10 | | | | | | | 0.8 | | |
| 0.12 | O | 0.004 | | | 4C | | 1.0 | | |
| 0.14 | -0.004 | or less | | | | | | | 1.0 |
| 0.16 | 0.004 | 01 1033 | | | | | 2.5 | | |
| 0.18 | | | | 6C | | 5.0 | 3.0 | | |
| 0.20 | | | | 00 | 6C | 7.0 | 3.0 | | |
| 0.23 | | | | | | | 3.5 | | |
| 0.26 | | | 2450~2750 | 8C | | 12.0 | 5.0 | | |
| 0.27 | | | 2100 2100 | 30 | | | 5.0 | | |
| 0.29 | O | | | | 8C | 8C | 80 | 15.0 | 8.0 |
| 0.30 | -0.007 | | | | | | | 20.0 | 10.0 |
| 0.32 | | | 2350~2650 | 10C | | 22.0 | 10.0 | | |
| 0.35 | | 0.005 | 2000 2000 | | | 22.0 | | | |
| 0.40 | | or less | | | 12C | 25.0 | 12.0 | | |
| 0.45 | | or iess | | | | | | | |
| 0.50 | | | 2300~2600 | 12C | | | | | |
| 0.55 | | | | 200 | | | | 30.0 | |
| 0.60 | O | | | | 40.0 | 00.0 | _ | | |
| 0.65 | -0.010 | | | | | | | | |
| 0.75 | 0.010 | | | | | 40.0 | | | |
| 0.80 | | | 2210~2500 | 16C | | 10.0 | | | |
| 0.90 | | 1 | | 100 | | 50.0 | _ | | |
| 1.00 | 0 | 0.007 | | | | 50.0 | | | |
| 1.20 | -0.015 | or less | 2110~2400 | 18C | | 60.0 | | | |
| 1.40 | 0.010 | or ress | 2060~2350 | 180 | | 60.0 | | | |
| 1.60 | | | 2010~2300 | 22C | _ | 120.0 | | | |
| 1.80 | | | 1960~2260 | 220 | | 120.0 | | | |
| 2.00 | O | 0.010 1910~2210 or less 1860~2160 | 1910~2210 | | | | | | |
| 2.30 | -0.020 | | 1860~2160 | 24C | | 130.0 | | | |
| 2.60 | | | 1810~2110 | 240 | | | | | |
| 2.90 | | 1770~2060 | | | | 150.0 | | | |

Remarks

: As to other specs than the standard specs, we'll discuss with you upon receiving your inquiry.

: As to less than 0.10 mm wire diameter, please see our pamphlet for "stainless steel wire SUPER FINE for

super fine spring".

4. Characteristics

4-1. Work hardening characteristic

Figures 1 to 3 show changes in tensile characteristic and torsional characteristic of Herculee and SUS304 in wire drawing processing.

Herculee shows higher values compared with SUS304 when measured with the same reduction of area (more than 60%), such as its tensile strength running at more than 300 N/mm², and its torsional strength running at more than 150 N/mm².

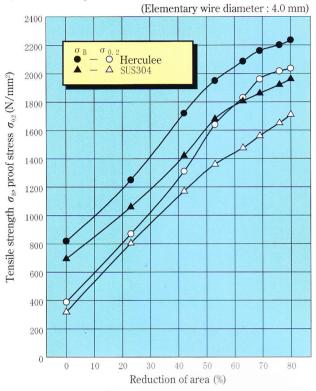


Fig. 1 Relation between reduction of area and $\sigma_{_{\rm R}}$ and $\sigma_{_{0.2}}$

Fig. 2 Relation between reduction of area and δ and ϕ

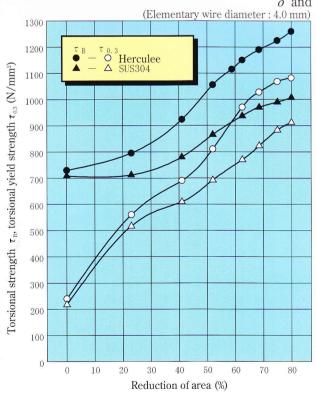


Fig. 3 Relation between reduction of area and $\tau_{\rm B}$ and $\tau_{\rm 0.3}$

4-2 low-temperature annealing characteristic

Cold-work hardened wire like austenite-based stainless steel wire is treated with low-temperature annealing, after spring is formed, allowing wire to restore tensile strength, hardness and elastic limit through removal of residual stress, for the purpose of reducing permanent set and further improving strength against fatigue.

Figures 4 through 6 show changes in tensile characteristic and torsional characteristic of Herculee and SUS30, which have been treated with low-temperature annealing for 30 minutes at every 50°C in the range of 300 to 500°C after going through wire drawing process.

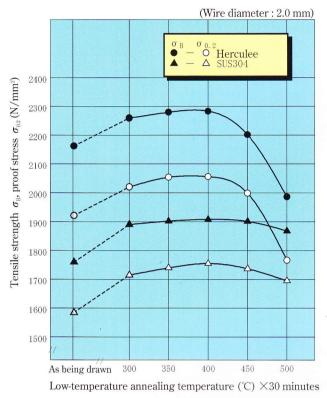


Fig. 4 Change in $\sigma_{\rm B}$ and $\sigma_{\rm 0.2}$ by low-temperature annealing

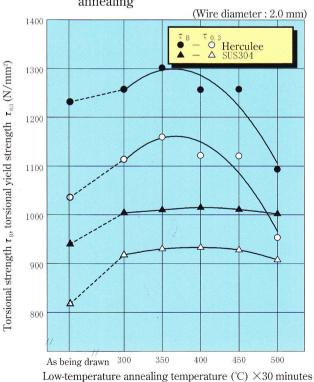


Fig. 6 Change in $\tau_{_{B}}$ and $\tau_{_{0.3}}$ by low-temperature annealing

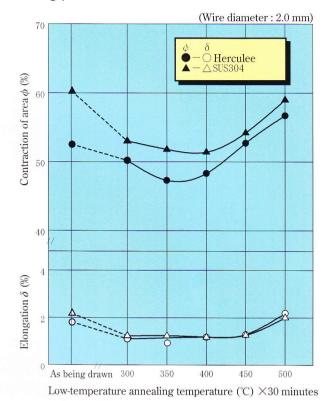


Fig. 5 Change in δ and ϕ by low-temperature annealing

Optimum condition of low-temperature annealing process for Herculee is $350^{\circ}\text{C} \times 30$ minutes, 50°C lower than $400^{\circ}\text{C} \times \text{minutes}$ for SUS304.

Tensile strength and 0.2% proof stress of Herculee after low-temperature annealing process show more than about 300 N/mm² higher than those of SUS304, and torsional strength and torsional yield strength show more than about 200 N/mm² higher.

In short, Herculee has strength and elastic limit equivalent to piano wire (SWP-B), and at the same time, it provides enough elongation and contraction of area (See Fig. 5) for spring usage.

Tables 3 and 4 show tensile characteristic and torsional characteristic of Herculee and comparative steel types like SUS304 and piano, during wire drawing process and optimum low-temperature annealing process (wire diameters 2.0 mm and 0.4 mm).

Table 3 Changes in mechanical characteristic caused by low-temperature annealing (Wire diameter 2.0 mm)

| Со | ndition | Tensile strength $\sigma_{\rm B}$ (N/mm ²) | Proof stress $\sigma_{0.2}$ (N/mm ²) | Modulus of elasticity E (kN/mm²) | Torsional strength $\tau_{\rm B}$ (N/mm ²) | Torsional yield strength $\tau_{0.3}$ (N/mm ²) | Modulus of rigidity G (kN/mm²) |
|----------|---------------------------|--|--|--|--|--|--------------------------------------|
| Herculee | In wire drawing process | 2157 | 1922 | 165.7 | 1236 | 1040 | 71.6 |
| nercuiee | Low-temperature annealing | 2285 | 2059 | 171.6 | 1304 | 1157 | 73.5 |
| CLICOOA | In wire drawing process | 1765 | 1589 | 161.8 | 941 | 814 | 68.6 |
| SUS304 | Low-temperature annealing | 1932 | 1755 | 166.7 | 1020 | 932 | 69.6 |
| SWP-A | In wire drawing process | 1893 | 1520 | 192.2 | 1089 | 863 | 78.5 |
| SWP-A | Low-temperature annealing | 2040 | 1863 | 205.9 | 1177 | 1030 | 80.4 |
| SWP-B | In wire drawing process | 2118 | 1706 | 194.2 | 1226 | 995 | 78.5 |
| 2WP-B | Low-temperature annealing | 2285 | 2059 | 206.9 | 1324 | 1128 | 80.4 |

Table 4 Changes in mechanical characteristic caused by low-temperature annealing (Wire diameter 0.4 mm)

| | | | | 8 (| Z | | |
|-----------|---------------------------|--|--|--|--|--|--------------------------------------|
| Condition | | Tensile strength σ_B (N/mm ²) | Proof stress $\sigma_{0.2}$ (N/mm ²) | Modulus of elasticity E (kN/mm²) | Torsional strength τ_B (N/mm ²) | Torsional yield strength $\tau_{0.3}$ (N/mm ²) | Modulus of rigidity G (kN/mm²) |
| Hamaulaa | In wire drawing process | 2623 | 2346 | 189.7 | 1373 | 1196 | 77.6 |
| Herculee | Low-temperature annealing | 2705 | 2461 | 194.5 | 1399 | 1234 | 79.1 |
| SUS304 | In wire drawing process | 2170 | 1931 | 173.5 | 1058 | 918 | 74.3 |
| 303304 | Low-temperature annealing | 2377 | 2139 | 179.2 | 1123 | 1025 | 75.1 |
| SWP-A | In wire drawing process | 2506 | 2284 | 185.7 | 1304 | 1006 | 77.9 |
| SWF-A | Low-temperature annealing | 2546 | 2328 | 193.1 | 1321 | 1137 | 79.6 |
| SWP-B | In wire drawing process | 2610 | 2348 | 187.7 | 1340 | 1025 | 78.2 |
| 2ML-B | Low-temperature annealing | 2641 | 2411 | 194.4 | 1356 | 1151 | 79.8 |

Low-temperature annealing condition Herculee

Herculee SUS304 : 350°C×30 minutes : 400°C×30 minutes

SWP-A, SWP-B: 200°C×30 minutes

4-3. Tensile strength standard

Table 5 shows comparison between tensile strength standards for Herculee depending on specific wire diameters and (JIS standards) for SUS304-WPB, piano wire Class A (SWP-A) and piano wire Class B (SWP-B).

Tensile strength standards for Herculee on thin wire diameter side are slightly lower than standards for piano wire (SWP-A), and on thick wire diameter side, standards are almost equivalent to those for SWP-B.

Table 5 Tensile strength standard

| Standard wire Tensile strength (N/mm²) | | | | | |
|--|--|--|---|--|--|
| | Tensile strer | ngth (N/mm²) | - | | |
| Herculee | SUS304-WPB | SWP-A | SWP-B | | |
| | | 2790~3090 | 3090~3380 | | |
| * | | 2750~3040 | 3040~3330 | | |
| 2550~2840 | 2150~ .2400 | 2700~2990 | 2990~3290 | | |
| 2000 - 2040 | 2130 - 2400 | 2650~2940 | 2940~3240 | | |
| | | 2600~2890 | 2890~3190 | | |
| | | 2600~2840 | 2840~3090 | | |
| | | 2550~2790 | 2790~3040 | | |
| $2450 \sim 2750$ | | 2500~2750 | 2750~2990 | | |
| | 2050 ~ .2200 | 2450~2700 | 2700~2940 | | |
| | 2030 - 2300 | 9400 9650 | 0.050 | | |
| $2350 \sim 2650$ | | 2400~2650 | 2650~2890 | | |
| | | 2350~2600 | 2600~2840 | | |
| | | 0000 0550 | 0==0 | | |
| 2300~2600 | 1950~2200 | 2300~2550 | $2550 \sim 2790$ | | |
| 2300 - 2600 | | 2260~2500 | 2500~2750 | | |
| | | 0010 015 | | | |
| | | $2210\sim2450$ | $2450 \sim 2700$ | | |
| | | 2160~2400 | 2400~2650 | | |
| $2210 \sim 2500$ | 1850~2100 | 2110~2350 | 2350~2600 | | |
| | | 2110~2300 | 2300~2500 | | |
| | | 2060~2260 | 2260~2450 | | |
| 2110~2400 | 1750 - 2000 | 2010~2210 | 2210~2400 | | |
| $2060 \sim 2350$ | 1750~2000 | 1960~2160 | 2160~2350 | | |
| 2010~2300 | | 1910~2110 | 2110~2300 | | |
| $1960 \sim 2260$ | $1650 \sim 1900$ | 1860~2060 | 2060~2260 | | |
| 1910~2210 | 8 | 1810~2010 | 2010~2210 | | |
| 1860~2160 | 1550 - 1000 | 1770 1000 | | | |
| 1810~2110 | 1000~1800 | 1770~1960 | 1960~2160 | | |
| 1770~2060 | $1450 \sim 1700$ | 1720~1910 | 1910~2110 | | |
| | Herculee $2550 \sim 2840$ $2450 \sim 2750$ $2350 \sim 2650$ $2300 \sim 2600$ $2210 \sim 2500$ $2110 \sim 2400$ $2060 \sim 2350$ $2010 \sim 2300$ $1960 \sim 2260$ $1910 \sim 2210$ $1860 \sim 2160$ $1810 \sim 2110$ | Tensile strer Herculee SUS304-WPB $2550\sim2840 \qquad 2150\sim2400$ $2450\sim2750 \qquad 2050\sim2300$ $2350\sim2650 \qquad 1950\sim2200$ $2210\sim2500 \qquad 1850\sim2100$ $2110\sim2400 \qquad 2060\sim2350 \qquad 2010\sim2300$ $1960\sim2260 \qquad 1950\sim1900$ $1910\sim2210 \qquad 1860\sim2160$ $1810\sim2110 \qquad 1550\sim1800$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | |

Remarks: As to in-between wire diameter, use value for standard wire diameter larger than that.

4-4. Corrosion resistance

Table 6 shows the results of tests, including nitric acid immersion test, sulfuric acid immersion test, ferric chloride immersion test and salt spray test specified by JIS, that were conducted on Herculee and SUS304, where these wires have been treated with optimum low-temperature annealing after the process of drawing.

Table 6 Result of corrosion resistance test

| Treath of the state of control of the control of th | | | | | | |
|--|----------|---|---|--|--------------------|--------------------------|
| Condition | | | Virgin 1 | | Ni plated material | |
| | | Nitric acid immersion test | Sulfuric acid immersion test | Ferric chloride immersion test | Salt spray test | |
| | | Corros | ion weight loss (g | /m²·hr) | Rust developme | ent area ratio (%) |
| In wire drawing | Herculee | 0.50 | 360 | 21 | 5~25 | 5~25 |
| process | SUS304 | 0.29 | 204 | 23 | 0~ 5 | 5~25 |
| Low-temperature | Herculee | 0.56 | 443 | 23 | 25~50 | 25~50 |
| annealing | SUS304 | 0.34 | 288 | 26 | 5~25 | 25~50 |
| Remarks | | 65% HNO ₃ Boiling×48 hr JIS G 0573 | 5% H ₂ SO ₄ Boiling×6 hr JIS G 0591 | 6%FeCl₃+1/20N HCl 35°C×24hr JIS G 0578 | 35℃× | NaCl <240hr Z 2371 |

Low-temperature annealing condition Herculee: 350°C×30 minutes, SUS304: 400°C×30 minutes

Slight difference in corrosion resistance of Herculee is allowed compared to SUS304, due to different contents of C, Cr and Ni.

However, corrosion resistance of Ni plated wires that are frequently used for spring material, are generally equivalent to that of SUS304.

4-5. Fatigue characteristic of wire

Figure 7 and Table 7 show the result of S-N diagram by Nakamura-type repetition rotary bending test, conducted on Herculee and SUS304 wires that have been straightened after being drawn.

As to fatigue limit at the time of 10⁷ times of repetitions, fatigue limit of Herculee is 564N/mm², 137N/mm² higher than that of SUS304.

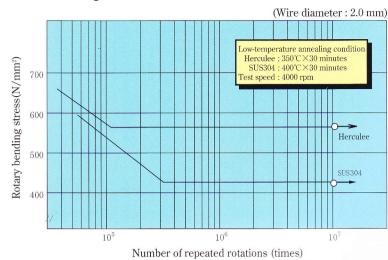


Table 7 Result of fatigue test of wire (Wire diameter 2.0 mm)

| Condition | Fatigue strength (N/mm²) | | | | Tensile strength |
|-----------|--------------------------|-----------------------|------------|--|---------------------|
| 10⁵ time | | 10 ⁷ times | (N/mm^2) | | |
| Herculee | 574 | 564 | 2206 | | |
| SUS304 | 539 | 427 | 1824 | | |

Low-temperature annealing condition Herculee: 350°C× 30 minutes SUS304: 400°C× 30 minutes

Fig. 7 Result of rotary bending test (Nakamura-type)

4-6. Fatigue characteristic of spring

Fig. 8 shows the result of spring fatigue test conducted on compression-coiled spring (wire diameter 1.0 mm) of Herculee and SUS304. Table 8 shows specs for spring used in the test.

When fatigue limit at the time of 10⁷ times of repetition is measured, with the average stress 490 N/mm² kept constant, Herculee shows 319 N/mm², satisfying about 50 N/mm² higher stress amplitude compared to SUS304.

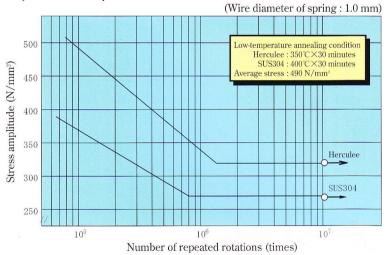


Fig. 8 Spring fatigue characteristic wear result

Table 8 Specs for compression coiled spring for fatigue test

| Wire diameter (mm) | 1.0 |
|------------------------------------|----------------|
| Average diameter of coil (mm) | 10.0 ± 0.1 |
| Total number of wire turns (turns) | 6.0 |
| Effective wire turns (turns) | 4.0 |
| Free length (mm) | 26.0 ± 0.2 |
| Squareness | 2° or less |

Figure 9 shows the result of spring fatigue test conducted on compression coiled spring (wire diameter 0.5 mm) of Herculee, and Figure 10 and Table 9 show the result of spring fatigue test, where shot peening is performed.

Table 10 shows specs for springs used in the test.

As to fatigue limit with average stress of 600 N/mm² kept constant, and 107 times of repetitions, it is found that fatigue limit can be substantially improved by performing shot peening. To be more specific, fatigue limit of 300 N/mm² without shot peening can be improved to 500 N/mm² by shot peening.

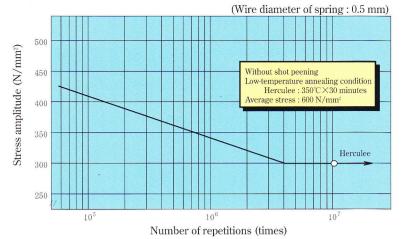


Table 9 Result of spring fatigue test

| | Fatigue limit (N/mm²) |
|------------------------|-----------------------|
| With shot peening | 600±500 |
| Without shot peening | 600±300 |
| Effect of shot peening | ±200 |

Fig. 9 Spring fatigue characteristic wear result (Without shot peening)

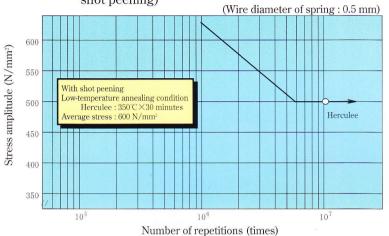


Table 10 Specs for compression coiled spring for fatigue test

| Wire diameter (mm) | 0.5 |
|------------------------------------|------------|
| Average diameter of coil (mm) | 4.0 |
| Total number of wire turns (turns) | 10.5 |
| Effective wire turns (turns) | 8.5 |
| Free length (mm) | 14.0 |
| Squareness | 2° or less |

Fig. 10 Spring fatigue characteristic wear result (With shot peening)

4-7. Permanent set characteristic of spring

Figure 11 shows the result of residual shearing distortion measurement after spring fatigue test with 107 times of repetitions (wire diameter 1.0 mm), to evaluate permanent set resistance.

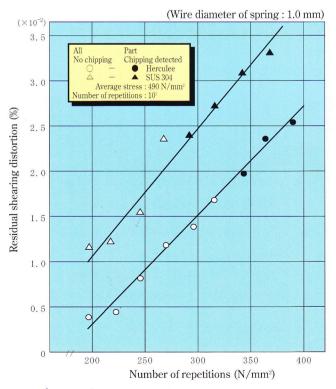


Fig. 11 Relation between stress amplitude and residual shearing distortion

Compared with SUS304, Herculee is extremely outstanding in its dynamic permanent set characteristic in spring, as residual shearing distortion (amount of distortion) within fatigue limit is as small as about 50 % or less.

4-8. Load characteristic of spring

A diagram showing load-to-distortion of tension springs of Herculee and SUS304 with fine wire diameter is shown in Figure 12, and Figure 13 shows a diagram as to Herculee and piano wire Class B (SWP-B).

Specification for the springs used in each test are as shown in Table 11 and Table 12.

Compared with SUS304, Herculee provides higher initial tension and higher load, and has the same load characteristic as that of piano wire Class B (SWP-B).

Table 11 Specs for tension spring for load-todistortion test

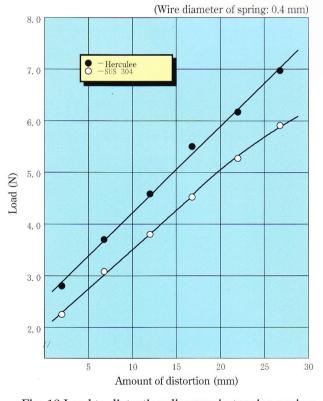
(For comparison between Herculee and SUS304)

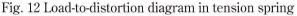
| (1 of comparison s | cerreen mercuree una be soon, |
|-------------------------------|-------------------------------|
| Wire diameter (mm) | 0.4 |
| Average diameter of coil (mm) | 2.9 |
| Number of wire turns (turns) | 50 · 1/4 |
| Free length (mm) | 43 |
| Low-temperature annealing | 280 +20 (°C) |
| processing | - 0 |

Table 12 Specs for tension spring for load-todistortion test

(For comparison between Herculee and SWP-B)

| Wire diameter (mm) | 0.4 |
|--------------------------------------|----------|
| Average diameter of coil (mm) | 3.0 |
| Number of wire turns (turns) | 52 · 1/4 |
| Free length (mm) | 46 |
| Low-temperature annealing processing | None |





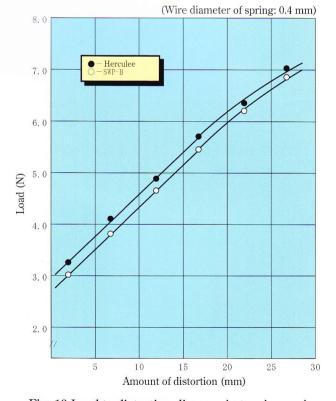


Fig. 13 Load-to-distortion diagram in tension spring

4-9. Permanent set characteristic of spring at high-temperature

Figure 14 shows the result of high-temperature tightening test of compression coiled springs (wire diameter 2.0 mm) of Herculee and SUS304.

Specs for the springs used in the test are as shown in Table 13.

High-temperature permanent set characteristic of Herculee spring is excellent because of its higher allowable stress compared with SUS304.

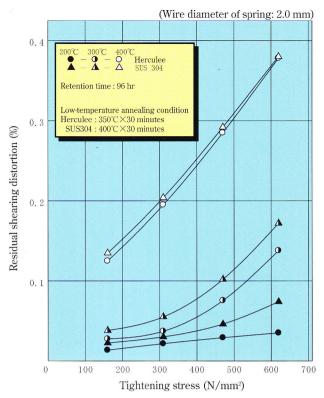


Fig. 14 Diagram showing deformation caused by spring fatigue at high temperature

Table 13 Specs for compression coiled spring for fatigue test

| 9 | | |
|--------------------------------------|---------------------------|--|
| Wire diameter (mm) | 2.0 | |
| Average diameter of coil (mm) | 18.5 ± 0.2 | |
| Total number of wire turns (turns) | 6.5 | |
| Effective wire turns (turns) | 4.5 | |
| Free length (mm) | 47.0 ± 0.3 | |
| Squareness | 2° or less | |
| Low-temperature annealing processing | Herculee:350°C×30 minutes | |
| | SUS304:400°C ×30 minutes | |

5. Examples of use

Since Herculee has excellent characteristics in terms of high strength, fatigue strength or permanent set resistance, Herculee is believed to be able to address the following cases;

- •where it is impossible for SUS304 to deal with design stress,
- where permanent set resistance is regarded as important
- •where replacing from piano wire, or hard steel wire due to corrosion resistance; and
- •where replacing from piano wire due to cost aspects of spring with fine wire diameter.

Table 14 Examples of use

| Automobile | Electrical machines/ | OA devices/ | Daily necessities/ |
|--|--|--|--------------------|
| | home electronics | IT-related | others |
| Radiator valve springCarburetor springKey ring | Breaker springDishwasher spring | Copying machine spring Connector spring Back-up taperelated spring Printer spring | Speed changer |